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Report of Investigations No. 38 1987

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Report of Investigations No. 38

## GEOTHERMAL RESOURCES OF THE WIND RIVER BASIN

Bern S. Hinckley ${ }^{1}$ by by Henry P. Heasler ${ }^{2}$



Laramie, Wyoming
1987

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## Conversion factors

Length

| Mass | 1 gallon per minute $=3.785$ liters per minute ( 1 pm ) |
| :---: | :---: |
| flow | 1 liter per minute $=0.2642$ gallon per minute (gpm) |
| Pressure | $\begin{aligned} 1 \text { pound per square inch } & =0.07031 \mathrm{kilogram} \mathrm{per} \text { square } \\ & \text { centimeter }\left(\mathrm{kg} / \mathrm{cm}^{2}\right) \\ & =0.06805 \text { atmosphere }(\text { atm. }) \end{aligned}$ |
|  | $\begin{aligned} 1 \text { kilogram per square centimeter } & =14.22 \text { pounds per square inch (psi) } \\ & =0.9678 \text { atm. } \end{aligned}$ |
| Thermal gradient | 1 degree Fahrenheit per thousand feet $=$ $=1.823$ degrees Celsius per kilometer ( ${ }^{\circ} \mathrm{C} / \mathrm{km}$ ) |
|  | ```1 degree Celsius per kilometer = 0.5486 }\mp@subsup{}{}{\circ}\mathrm{ Fahrenheit per thousand``` feet ( ${ }^{\circ} \mathrm{F} / 1,000 \mathrm{ft}$ ) |

Thermal $\quad 1$ millicalorie per centimeter per second per degree Celsius conductivity $\left(10^{-3} \mathrm{cal} / \mathrm{cm} \mathrm{sec}{ }^{\circ} \mathrm{C}\right)=$
$=241.8$ British thermal units per foot per hour per degree Fahrenheit (Btu/ft hr ${ }^{\circ}$ F)
$=0.418$ watt per meter per degree Kelvin ( $\mathrm{W} / \mathrm{m}^{\circ} \mathrm{K}$ )

Heat $\quad 1$ microcalorie per square centimeter per second $\left(10^{-6} \mathrm{cal} / \mathrm{cm}^{2} \mathrm{sec}\right)=$
flow
$=1$ heat flow unit (HFU)
$=0.013228$ British thermal unit per square foot per hour (Btu/ft ${ }^{2} \mathrm{hr}$ )
$=41.8$ milliwatts per square meter $\left(10^{-3} \mathrm{~W} / \mathrm{m}^{2}\right.$ or $\left.\mathrm{mW} / \mathrm{m}^{2}\right)$

Temperature 1 degree Fahrenheit $=0.56$ degree Celsius $\left({ }^{\circ} \mathrm{C}\right)$
$1^{\circ} \mathrm{Cel}$ sius $=1.8^{\circ} \mathrm{Fahrenheit}\left({ }^{\circ} \mathrm{F}\right)$
${ }^{\circ} \mathrm{F}=1.8^{\circ} \mathrm{C}+32 \quad{ }^{\circ} \mathrm{C}=\left({ }^{\circ} \mathrm{F}-32\right) / 1.8$

## Introduction

This is the fourth in a series of reports describing the geothermal resources of Wyoming basins (Figure 1). Each basin report contains a discussion of hydrology as it relates to the movement of heated water, a description and interpretation of the thermal regime, and four maps (Sheets 1 through 4, back pocket): a generalized geological map (Sheet 1), a thermal gradient contour map (Sheet 2), a structure contour map (Sheet 3), and a ground-water temperature map (Sheet 4). The format of these reports varies, as does the detail of interpretation, because the type of geothermal system, quantity and reliability of thermal data, and amount of available geologic information vary substantially between basins and between areas within basins.

This introduction contains (1) a general discussion of how geothermal resources occur, (2) a discussion of the temperatures, distribution, and possible applications of geothermal resources in Wyoming and a general description of the State's thermal setting, and (3) a discussion of the methods used in assessing the geothermal resources. This introduction is followed by a description of the geothermal resources of the Wind River Basin of central Wyoming (Figure 1).

Funding for this project was provided


Figure 1. Study areas planned or completed in this serles.
by the U. S. Department of Energy to the Wyoming Geothermal Resource Assessment Group under Cooperative Agreement DE-F107-79ID12026 with the University of Wyoming Department of Geology and Geophysics, and by the Wyoming Water Research Center. Compilations of oilwell bottom-hole temperatures can be examined at the office of the Geological Survey of Wyoming in Laramie.

The text uses primarily British units. As outlined in footnotes on the following page, heat flow and thermal conductivity data are generally presented in metric units. A table of conversion factors faces this page.

## Geothermal systems and resources

In this report a geothermal resource is heated water close enough to the earth's surface to be useful. Further definitions or classifications of geothermal resources are not attempted here because they are based on changing technological and economic parameters. Rather, we use geothermal data to describe the thermal regime in each basin. Thermal anomalies are identified, but no
attempt is made to determine to what degree an anomaly is a resource.

Geothermal systems vary from hightemperature, steam-dominated, naturally pressurized types to warm water, mechan-ically-pumped systems. The type of system depends on how the heat flowing out of the earth is modified by complex geologic and hydrologic conditions. Common-
$1 y$, the earth warms up about $14^{\circ} \mathrm{F}$ for every 1,000 feet of depth (Anderson and Lund, 1979). An attractive geothermal resource may exist where the thermal gradient is significantly higher than $14^{\circ} \mathrm{F} / 1,000$ feet.

Heat-flow studies in Wyoming basins (Decker and others, 1980; Heasler and others, 1982) have reported heat flows of 33 to 80 milliwatts per square meter (mW/m ${ }^{2}$ ) (Figure 2). The most notable exception is in the northwest corner of Wyoming, in Yellowstone National Park, where very high heat flows of over 105 $\mathrm{mW} / \mathrm{m}^{2}$ (Morgan and others, 1977) result in high-temperature water at shallow depth.

By itself, a background heat flow of 33 to $80 \mathrm{~mW} / \mathrm{m}^{2}$ does not suggest a significant geothermal resource. In Wyoming basins, the primary mechanism for translating moderate heat flow into abovenormal temperature gradients is groundwater flow through geologic structures. Figures 3 and 4 illustrate systems based on two different structural regimes. Ground water flowing downward from the recharge area equilibrates with the temperature of the surrounding rock. But locally, folded permeable rocks (Figure
3) or faults (Figure 4) provide conduits for this heated water to rise rapidly toward the surface. If water proceeds through such a conduit without major heat dissipation, an elevated thermal gradient develops. In Figures 3 and 4, the temperatures listed in the axes of synclines represent an undisturbed temperature increase with depth. Bold type values demonstrate rock temperatures increased by groundwater flow. Any natural or man-made zone through which water can rise, such as an extensive fracture system or deep drill hole, serves the same purpose.

Because warm water is less dense than cold water, geothermally heated water tends to rise, a process known as free convection. Free convection is relatively weak, and is significant only under conditions of extreme temperature difference or relatively unrestricted flow. Forced convection occurs where water moves in a confined aquifer from an elevated recharge area at a basin margin to a lower discharge area. Water is forced over folds or up faults, fractures, or wells by the artesian pressure developed within the confined aquifer. Forced convection is more important in Wyoming basins than free convection.

Temperature, distribution, and application of resources

Renner and others (1975), of the U.S. Geological Survey, divide geothermal systems into three groups: (1) hightemperature systems, greater than $302^{\circ} \mathrm{F}$ ( $150^{\circ} \mathrm{C}$ ); (2) intermediate-temperature systems, $194-302^{\circ} \mathrm{F}\left(90-150^{\circ} \mathrm{C}\right)$; and (3) low-temperature systems, less than $194^{\circ} \mathrm{F}$ $\left(90^{\circ} \mathrm{C}\right)$. While Yellowstone National Park is a high-temperature system, the sedimentary basins of Wyoming fall mostly into the low-temperature and interme-diate-temperature groups.

Due to the great depth of many Wyoming basins, ground water at elevated temperature exists beneath vast areas of the State (Heasler and others, 1983). Where systems like those described in

Pigures 3 and 4 create local areas of high gradient, it may be feasible to develop the shallow geothermal resource directly. Outside these scattered areas of high thermal gradients, geothermal development will probably depend upon much deeper drilling, such as that provided by oil and gas exploration.

The geothermal resources in the basins are suited to relatively smallscale, direct-use projects located close by. Energy uses include a wide range of space heating, agricultural, aquacultural, and low-temperature processing applications. (See Anderson and Lund, 1979, for a discussion of direct-use geothermal applications.) Below $100^{\circ} \mathrm{F}$,

Explanation

| Heat-flow determinations $\left(\mathrm{mW} / \mathrm{m}^{2}\right)$ |  |
| ---: | :--- | ---: |
| $\Delta<35$ | $\square 4-85$ |
| $\square 36-48$ | $\bullet 86-102$ |
| $049-60$ | $\otimes>103$ |
| $\Delta 61-73$ |  |



Figure 2. Generalized geology and generalized heat flow in Wyoming and adjacent areas, showing sedimentary basin areas defined in this series of reports to be underlain by water warmer than $120^{\circ} \mathrm{F}$ (after Heasler and others, 1983). Yellowstone National Park and Jackson Hole were not investigated.

Mountain
outcrops


Figure 3. Simplified cross section of a typlcal Wyoming fold-controlled geothermal system. Arrows indicate flow of ground water.


Figure 4. Simplified cross section of a typical Wyoming fault-controlled geothermal system. Arrows Indicate flow of ground water.
uses are limited to such applications as soil and swimming pool warming, deicing and fish farming. Through the use of ground-water heat pumps, energy can be extracted from natural waters as cool as $40^{\circ} \mathrm{F}$ (Gass and Lehr, 1977).

The presently documented thermal springs in the State's basin areas (Breckenridge and Hinckley, 1978; Heasler and others, 1983) release 3.5 trillion British thermal units (Btu's)
of heat per year in cooling to ambient temperature. Like the oil springs and seeps that led developers to Wyoming's vast petroleum fields, thermal springs are simply the surface manifestation of the much larger, unseen geothermal resource. For example, Hinckley (1984) calculated that approximately 24 trillion Btu's of heat would be released per year if all the thermal water produced as a by-product in Wyoming oil fields cooled to ambient temperature.

The principal purpose of these reports is the documentation and prediction of temperatures in the subsurface. In sections above, we have established a qualitative framework in which higher-than-expected thermal gradients occur where deep-heated water moves to shallow depth. Quantification of temperatures and gradients required a variety of techniques. Sources of subsurface temperature data include: (1) thermal logs of wells; (2) oil and gas well bottomhole temperatures; and (3) surface temperatures of springs and flowing wells.

## Thermal logs of wells

Thermal logs of wells are the most reliable data on subsurface temperatures because they represent direct measurements under thermally stable conditions. Using thermistor probes precise to $+0.005^{\circ} \mathrm{C}$ (Decker, 1973), the Wyoming Geothermal Resource Assessment Group has obtained temperature measurements in over 380 holes across Wyoming (Heasler and others, 1983). Temperatures were measured at intervals of 32 feet or less in holes up to 6,500 feet deep. Many of the logged holes had had years to equilibrate, so temperatures of sampled intervals approached true rock temperatures. With these temperature-depth data, least-squares statistical analysis was used to determine gradients at depths below the effects of long-term and short-term surface temperature fluctuations. These values are accepted as the most reliable thermal gradients, to which other temperature and gradient information is compared.

Where rock samples from a logged hole were available for testing, laboratory determinations of thermal conductivity were made. Decker (1973) discusses the laboratory techniques used for thermal conductivity determination. This information, coupled with the measured gradients, was used to calculate local heat flow. Where stratigraphic relationships
or multiple holes with similar heat flow allowed us to rule out hydrologic disturbance, we could determine a purely conductive heat flow. This heat flow was, in turn, applied to all sequences of strata for which thermal conductivities could be estimated to obtain gradient values in the absence of holes that could be logged. Particularly in the deeper portions of Wyoming sedimentary basins, this technique was used as a semiquantitative check on less reliable data.

## $0 i 1$ and gas well bottom-hole temperatures

Oil and gas well bottom-hole temperatures (BHTs) are the most abundant subsurface temperature data. Because of their abundance, BHTs were used to assess geothermal resources in this study. Over 14,000 oil and gas well bottom-hole temperatures have been collected for the study areas (Table 1). Thermal gradients were calculated from BHT information using the formula:

$$
\text { Gradient }=\frac{\text { BHT }-\begin{array}{l}
\text { Mean annual } \\
\text { air temperature }
\end{array}}{\text { Depth }}
$$

Mean annual air temperatures for Wyoming basins are between $40^{\circ}$ and $48^{\circ} \mathrm{F}$ (Lowers, 1960). These values, assumed to approximate mean annual ground temperatures, were used in calculating gradients over fairly large areas. This procedure assumes that variations due to elevation and microclimatic effects are negligible compared with BHT inaccuracies. Well log data on file at the Geological Survey of Wyoming were the principal source of BHT data. (A slightly larger data base is available at the Wyoming Oil and Gas Conservation Commission Office in Casper, Wyoming.)

The use of oil field bottom-hole temperatures in geothermal gradient studies is the subject of some controversy among

Table 1. Summary of geothermal data on Wyoming sedimentary basins.

| Basin: | Bighorn | Great <br> Divide and Washakie | Green River | Laramie, Hanna and Shirley | Southern Powder River | Wind River |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Number of bottomhole temperatures analyzed. | 2,035 | 1,880 | 1,530 | 445 | 6,100 | 1,740 |
| Number of wells thermally logged. | 70 | 68 | 47 | 57 | 60 | 67 |
| Background thermal gradient in ${ }^{\circ} \mathrm{F} / 1,000$ feet ( ${ }^{\circ} \mathrm{C} /$ kilometer). | $\begin{gathered} 16 \\ (29) \end{gathered}$ | $\begin{gathered} 15 \\ (27) \end{gathered}$ | $\begin{gathered} 13 \\ (24) \end{gathered}$ | $\begin{gathered} 12-15 \\ (22-28) \end{gathered}$ | $\begin{gathered} 14 \\ (25) \end{gathered}$ | $\begin{gathered} 15 \\ (28) \end{gathered}$ |
| Highest recorded temperature and corresponding depth. | $\begin{gathered} 206^{\circ} \mathrm{F} \text { at } \\ 23,000 \mathrm{ft} \\ \left(152^{\circ} \mathrm{C}\right. \text { at } \\ 2,035 \mathrm{~m}) \end{gathered}$ | $\begin{aligned} & 376^{\circ} \mathrm{F} \text { at } \\ & 24,000 \mathrm{ft} \\ & \left(191^{\circ} \mathrm{C}\right. \text { at } \\ & 7,300 \mathrm{~m}) \end{aligned}$ | $\begin{aligned} & 306^{\circ} \mathrm{F} \text { at } \\ & 21,200 \mathrm{ft} \\ & \left(152^{\circ} \mathrm{C}\right. \text { at } \\ & 6,453 \mathrm{~m}) \end{aligned}$ | $\begin{aligned} & 223^{\circ} \mathrm{F} \text { at } \\ & 12,000 \mathrm{ft} \\ & \left(106^{\circ} \mathrm{C}\right. \text { at } \\ & 3,600 \mathrm{~m}) \end{aligned}$ | $\begin{aligned} & 275^{\circ} \text { at } \\ & 16,000 \mathrm{ft} \\ & \left(135^{\circ} \mathrm{C}\right. \text { at } \\ & 4,900 \mathrm{~m}) \end{aligned}$ | $370^{\circ} \mathrm{F}$ at <br> 21,500 ft <br> ( $188^{\circ} \mathrm{C}$ at <br> $6,55 \mathrm{~m}$ ) |
| Basin depth in feet (kilometers). | $\begin{array}{r} 26,000 \\ (8.0) \end{array}$ | $\begin{array}{r} 26,000 \\ (8.5) \end{array}$ | $\begin{array}{r} 30,200 \\ (9.2) \end{array}$ | $\begin{array}{r} 12,000 ; \\ 39,000 ; \\ 8,200 \\ (3.7 ; \\ 12.0 ; \\ 2.5) \end{array}$ | $\begin{gathered} 16,400 \\ (5.0) \end{gathered}$ | $\begin{array}{r} 25,800 \\ (7.6) \end{array}$ |

geothermal researchers. Problems associated with the thermal effects of drilling and with operator inattention in measuring and reporting BHTs cast doubt on the accuracy of individual temperature reports. It has been suggested, for example, that in some areas BHTs may correlate with the ambient air temperature during drilling and, specifically, that many of the thermometers used in the summer are reading their maximum temperature before they are lowered down the drill hole. Similarly, drilling fluids may transfer heat to the bottom of a drill hole, warming or cooling the rock depending on the drilling fluid temperature and the depth of the hole. The magnitude of a thermal disturbance depends on the temperature difference between the drilling fluid and the rock; the time between the end of fluid circulation and temperature measurement;
the type of drilling fluid used; the length of time of fluid circulation; and the degree to which drilling fluids have penetrated the strata.

Theoretical analysis of the deviation of a reported BHT from true formation temperature may be possible on a detailed, well-by-well basis, but is an overwhelming task basinwide. Therefore, for these studies it was assumed that such factors as time of year, operator error, time since circulation, and drilling fluid characteristics are random disturbances that average out over a large number of BHTs. The fact that drilling fluids are circulating, acting to homogenize temperatures within the hole, is, on the other hand, a systematic effect that depresses temperature more with increasing depth. 'With sufficient data at all depths, anomalous gradients may be
identified despite the fact that they are depressed in value.

The following procedure was used to assess geothermal resources in a basin from oil and gas well bottom-hole temperatures: First, all available BHTs were compiled and gradients were calculated. The gradients were then plotted on a map and contoured for the basin. Thermally logged holes define fixed points in the contouring.

As explained above, temperature gradient values may be lower in deeper holes because of drilling effects. This was taken into account in identifying gradient anomalies by grouping all temperature and gradient data for a basin into 500-foot depth intervals and then calculating the mean value and the 50 th , 66 th , 80th, and 90 th percentiles for each interval. These calculations are tabulated in each basin report. The 80 th percentile - the value below which 80 percent of the data fall - was chosen arbitrarily as a cutoff for the identification of geothermal anomalies.

A single background thermal gradient was calculated for each basin (Table 1), based on thermal logs, thermal conductivities of the basin's sedimentary sequence, and heat flow. Although BHT gradients are assumed to be depressed with depth, we do not feel that we can define as anomalous those gradients that are lower than the background thermal gradient. Therefore, thermal gradient values are identified as anomalous only if they fall above the 80th percentile for their depth range and above the background thermal gradient for the basin in which they occur.

In these basin studies, a lower BHT cutoff of $100^{\circ} \mathrm{F}$ was used. In our experience, a temperature gradient based on a temperature lower than $100^{\circ} \mathrm{F}$ is usually not reliable. Also, sub $-100^{\circ} \mathrm{F}$ water is of little economic value unless it occurs at very shallow depth.

The final criterion for identification of an area of anomalous gradient is
that a group of anomalous points (determined as outlined above) occur in the same area.

Particularly above and within zones of ground-water movement, gradients defined from bottom-hole temperatures may not completely reflect the character of a geothermal resource. For example, Figure 5 shows the effect of groundwater movement homogenizing temperatures in the lower portion of a hole at the top of the Thermopolis anticline. A gradient calculated from a single BHT at 800 feet would miss the very high gradients and temperatures in the top part of the hole. Conversely, a gradient calculated from a BHT at 400 feet would give a seriously erroneous temperature at 600 feet. These effects illustrate the importance of thermal logging in areas of suspected hydrologic disturbance. As a general check on the downward projection of thermal gradients, we know from heat flow and rock thermal conductivity considerations that gradients among the Wyoming basins are all similar below levels of hydrologic disturbance.

Temperature ${ }^{\circ} \mathrm{F}$


Figure 5. Temperature-depth plot showing hydrologic disturbance, based on a thermal log of a well at Thermopolis (from Hinckley and others, 1982).

An additional constraint on the use of gradient data to evaluate geothermal resources is that ground water must be present to transport the heat. Therefore, we have identified for each basin a productive, basinwide aquifer that is deep enough to contain water at useful temperatures, and for which thermal and hydrologic data are available. A map of temperatures within that aquifer, on which BHTs of that formation are plotted and contoured, is included in each basin report. Verification is provided by the sparse thermal-logging data. No attempt was made to correct BHTs for drilling effects, so a certain degree of underestimation of temperatures may be expected in the deeper zones, as described above. The deviation of BHTs from true formation temperatures is not known; however, a drill hole in an aquifer with active circulation should equilibrate to undisturbed temperatures relatively rapidly.

## Surface temperatures of springs and flowing wells

Surface temperatures of springs and flowing wells provide the third source of subsurface temperature data. The amount of cooling before the water reaches the surface is generally unknown; therefore, they provide only a minimum temperature check on BHT data. There is also commonly some uncertainty about the depth and source of flow. One can assume that all flow is from the bottom of a flowing well to obtain a minimum gradient. The most useful subsurface temperature data from springs and wells come from those whose source aquifer can be determined.

The most important aspect of any geothermal resource is the temperature and flow rate that can be delivered to the surface. In this sense, flowing wells and springs give excellent data. Selected locations of surface discharge of thermal water (greater than $70^{\circ} \mathrm{F}$ ) are indicated on the thermal gradient maps.

## Summary

The authors investigated the geothermal resources of several Wyoming sedimentary basins. Oil-well bottom-hole temperatures, thermal logs of wells and heat flow data were interpreted within a framework of geologic and hydrologic constraints. Basic thermal data, which includes the background thermal gradient and the highest recorded temperature and corresponding depth for each basin, are provided in Table 1.

These investigations of the geothermal resources of Wyoming sedimentary basins have resulted in two main conclusions:
(1) Large areas in Wyoming contain ground water at temperatures greater than $120^{\circ} \mathrm{F}$ (Figure 2). Although much of this water is too deep to be economically tapped solely for geothermal use, oil and gas wells may provide access to this significant geothermal resource.
(2) Isolated areas of high temperature gradients exist within each basin. These areas -- many revealed by hot springs -- represent geothermal systems that might presently be developed economically.

# Geothermal resources of the Wind River Basin, Wyoming 

## Geologic and hydrologic setting

## Stratigraphy

The Wind River Basin covers approximately 8,000 square miles in central Wyoming (see Figure 1 for location). Most of Fremont County and the eastern one-third of Natrona County are in the Wind River Basin.

In the Wind River Basin, the mass transfer of heat by moving water creates areas of high geothermal gradients. Therefore, it is important to identify those strata with favorable waterbearing characteristics. In addition, the confining strata above and below these aquifers must be considered in terms of their effectiveness in restricting ground-water flow patterns.

Sheet 1 presents the surface distribution of the various strata to be discussed. The stratigraphic chart for the Wind River Basin (Table 2) lists formation thicknesses, lithologies, general water-bearing characteristics, and water quality. Much of these data were taken from Richter (1981), to whom the reader is referred for a thorough discussion of Wind River Basin hydrogeology. Table 2 identifies strata as major confining units, confining units, aquifers, or major aquifers. These divisions are very general. Locally, in areas of relatively higher permeability and(or) small water demand, any formation listed may constitute a useful aquifer.

The youngest deposits in the Wind River Basin are the unconfined Quaternary sands, silts, and gravels deposited along stream channels. Because of their easy accessibility, good recharge, and generally high permeabilities, these deposits form one of the most important
aquifers in the basin. Ground-water temperature in this aquifer will generally approximate the mean annual air temperature $\left(43^{\circ} \mathrm{F}\right.$ for most of the Wind River Basin; Lowers, 1960). Such waters have geothermal potential primarily through the use of ground-water heat pumps. These devices can extract heat from any above-freezing waters and are therefore constrained more by general ground-water availability than by the distribution of geothermal anomalies.

Oligocene, Miocene, and Pliocene rocks are present only locally in the basin and in the Granite Mountains region. Like the Quaternary deposits, they are primarily unconfined aquifers. This lack of confinement precludes development of deep, forced-circulation systems like those depicted in Figures 3 and 4. These aquifers are therefore unlikely to provide waters of elevated temperature.

The Eocene Wagon Bed, Tepee Trail, and Aycross Formations are poor water producers and occur only in very limited, higher elevation areas in the extreme northwest and southeast parts of the basin. Both the lithology and the location of these formations preclude deep circulation of ground water; thus, there is little geothermal potential.

The Eocene Wind River Formation covers most of the surface of the Wind River Basin. The highly productive sandstones of this aquifer account for approximately 50 percent of all private domestic wells in the basin. An additional 30 percent are developed in Quaternary deposits (Richter, 1981). Although the Wind River Formation is mostly unconfined, interbedded low-

Table 2. Stratigraphic column for the Wind River Basin and Granite Mountains. 1

| Age | Formation | Thlckness <br> (In feet) | Lithologles | Water-bearling propertles | Water quallity ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Cenozole Quaternary | Undlvided | 0-100 | Unconsolldated clay, silt, sand, and gravel | Major aquifer: ylelds 5-5,000 gpm | TDS: $100-1,000 \mathrm{mg} / 1$ |
| Tertlary Pllocene | Moonstone Formation ${ }^{3}$ | 0-1,400 | Poorly consolldated shale, sandstone, mudstone, tuff, IImestone, conglomerate | $\frac{\text { Major aquifer: yields up to }}{500 \mathrm{gpm}}$ | TDS ${ }^{4} 100-1,000 \mathrm{mg} / \mathrm{l}$ |
| Miocene | Mlocene rocks ${ }^{5}$ | 0-900 | Sandstone with interbedded tuff, Itmestone, and conglomerate; basal conglomerate | Aquifer: yields $\leq 100 \mathrm{gpm}$ Major aquifer: yTelds generally up to $300 \mathrm{gpm}, 100 \mathrm{gpm}$ not uncommon | TDS $6600 \mathrm{mg} / 1$; Ca , $\mathrm{Na}, \mathrm{HCO}_{3}, \mathrm{SO}_{4}$ |
| Ol İgocene | White River Formation | 0-1,000 | Fine sandstone with interbedded tuff and bentonite | $\frac{\text { Aquifer: }}{850 \mathrm{gpm}} \text { yields } 1-300 \mathrm{gpm} \text {, maximum }$ |  |
| Eocene | Wagon Bed Formation | 0-700 | Bentonitic sandstone | Confining unit: ylelds < 10 gpm | TDS 1,500-2,500 mg/1 |
| Eocene | Tepee Trall formation | 0-2,000 | Tuffaceous siltstone, sandstone | Confining unit: ylelds $<10 \mathrm{gpm}$ |  |
| Eocene | Aycross Formation | 0-1,000 | Shale, mudstone, conglomerate, volcanics, sandstone | Confining unit |  |
| Eocene | WInd River Formation | 250-1,000 | Siltstone, shale, mudstone, sandstone | Major aquifer: ylelds up to 1,500 gpm, 200 gpm flowing wells | $\begin{aligned} & \text { TDS } 100-5,000 \mathrm{mg} / 1 ; \\ & \mathrm{HCO}_{3}, \mathrm{SO}_{4} \end{aligned}$ |
| Eocene | Indian Meadows Formation | - 0-700 | Mudstone, sandstone, 11 mestone | Confining Unit: |  |
| Paleocene | Fort Union Formation | 0-8,000 | Conglomerate, sandstone, shale, siltstone | Aquifer: ylelds up to $100 \mathrm{gpm}, 10$ gpm flowing wells. Basal section is a Confining unlt |  |
| Mesozolc Cretaceous | Lance Formatlon | 0-6,000 | Sandstone, shale, pebble conglomerate | Aquifer: yields up to 100 gpm | TDS $>1,000 \mathrm{mg} / \mathrm{I}$; Na , $\mathrm{SO}_{4}, \mathrm{Cl}, \mathrm{HCO}_{3}$ |
| Cretaceous | Meeteetse Formation | 0-1,300 | Sandstone, shale, slltstone, mudstone | Confining unit | poor |
| Cretaceous | Mesaverde Formation | 600-2,000 | Upper unit sandstone; middle unlt shale, siltstone, sandstone; basal sandstone | Aquifer: ylelds up to 500 gpm , Tocally arteslan | TDS $>1,500 \mathrm{mg} / 1$; Na , $\mathrm{SO}_{4}, \mathrm{HCO}_{3}$ |
| Cretacoous | Cody Shale | 3,000-5,500 | Shale with interbedded thin sandstones | Major confining unit | poor |
| Cretaceous | Frontler Formation | 500-1,000 | Alternating sandstone and shale | Aquifer: ylelds up to 150 gpm , $10-25 \mathrm{gpm}$ flowing wells | $\begin{aligned} & \text { TDS } 500-3,000 \mathrm{mg} / 1 ; \\ & \mathrm{Na}, \mathrm{SO}_{4}, \mathrm{HCO}_{3}, \mathrm{Cl} \end{aligned}$ |
| Cretaceous | Mowry Shale | 400-600 | Interbedded shale and bentonite | Major confining unit |  |
| Cretaceous | Muddy Sandstone | 20-150 | Fine- to medium-grained sandstone | Aquifer: $10-50 \mathrm{gpm}$ flowing wells | TOS $>500 \mathrm{mg} / 1 ; \mathrm{Cl}, \mathrm{H} \mathrm{O}_{3}$ |
| Cretaceous | Thermopolis Shale | 120-250 | Shale and mudstone, sandstone lenses | Major confining unit |  |
| Cretaceous | ```Cloverly Formation and Morrison Formation``` | $\begin{aligned} & 300 \\ & \text { to } \\ & 600 \end{aligned}$ | Sandstone, middle shale unlt Mudstone and shale, sandstone lenses | Aquifer: ylelds generally $<50 \mathrm{gpm}$, up to $300 \mathrm{gpm}, 1,025 \mathrm{gpm}$ flowing vells Confining unlt: ylelds $<5 \mathrm{gpm}$ | $\begin{aligned} & \mathrm{TDS}<1,500 \mathrm{mg} / 1 ; \mathrm{Na}, \\ & \mathrm{HO} 0_{3}, \mathrm{SO}_{4} \end{aligned}$ |
| Jurassic | Sundance Formation | 150-600 | Sandstone and stiltstone, carbonates at base | Aquifer: $250-500 \mathrm{gpm}$ flowing wells from Sundance-Nugget aquifer | $\begin{aligned} & \mathrm{TDS}<500-2,000 \mathrm{mg} / \mathrm{I} ; \\ & \mathrm{Na}, \mathrm{C1}, \mathrm{SO}_{4} \end{aligned}$ |
| Jurassic | Gypsum Spring Formation | 0-230 | Alternating siltstone, shale, IImestone, gypsum | Confining unit | poor |
| Jurassic | Nugget Sandstone | 0-400 | Fine to medlum sandstone, siltstone at base | Aquifer: artesian conditions common | $\begin{aligned} & \text { generally }>1,000 \mathrm{mg} / 1 \text {; } \\ & \mathrm{Na}, \mathrm{C1}, \mathrm{SO}_{4} \end{aligned}$ |
| Triassic | Chugwater Formation | 1,000-1,300 | Interbedded silitstone, sandstone, and shale | Major confining unit: sandstone layers locally yleld <20 gpm | generally poor, sandstone layers may have $T D S<1,000 \mathrm{mg} / 1$ |
| Triassic | DInwoody Formation | 0-250 | Interbedded siltstone, sandstone, and 1 imestone | Confining unit |  |
| Paleozolc |  |  |  |  |  |
| Permi an | Phosphorla Formatlon ${ }^{6}$ | 150-300 | Interbedded 1 imestone, dolomite, slitstone, sandstone; Increasing shale content eastward. | Aquifer: ylelds up to 100 gpm | TDS $<100 \mathrm{mg} / 1$; $\mathrm{Mg}, \mathrm{Ca}$, $\mathrm{Na}, \mathrm{HCO}_{3}, \mathrm{SO}_{4}$ |
| Pennsy I vantan | Tensleep Sandstone | 200-600 | Massive fine sandstone | $\frac{\text { Major aquifer: }}{\text { flowing wells }}$ up to $3,000 \mathrm{gpm}$ | TDS $<500 \mathrm{mg} / 1$ near outcrops; TDS $>2,000$ $\mathrm{mg} / \mathrm{I}$ In basin Interior; $\mathrm{Mg}, \mathrm{Ca}, \mathrm{Na}, \mathrm{HCO}_{3} \mathrm{SO}_{4}$ |
| Pennsylvanlan | Amsden Formation | 0-400 | Shale, Ilmestone, dolomlte; basal sandstone |  |  |
| Mississipplan | Madison Limestone | 200-700 | LImestone, dolomite; cavernous near top | Aquifer: ylelds 1-300 gpm | TDS $<500 \mathrm{mg} / 1$ |
| Devonlan | Darby Formation | 0-300 | Dolomite, slitstone, shale | $\frac{\text { Confining unit: }}{\text { fractured }}$ ylelds springs where |  |
| Ordoviclan | Bighorn Dolomite | 0-300 | Doloalte; basal sandstone | Aquifer |  |
| Cambrian | Gallatin LImestone | 0-450 | LImestone, shale, thin sandstone beds | Confining unit: ytelds $<5 \mathrm{gpm}$ |  |
| Cambrlan | Gros Ventre Formation | 0-750 | LImestone, shale | Confining unit |  |
| Cambrlan | Flathead Sandstone | 50-500 | Sandstone, basal conglomerate | Aquifer: ylelds 1-25 gpm | TDS $<500 \mathrm{mg} / \mathrm{I}$; $\mathrm{Ca}, \mathrm{Na}$, $\mathrm{SO}_{4}, \mathrm{HCO}_{3}$ |
| Precambrian |  | unknown | granite, gnless, schist | Small y yelds where fractured | good |

[^1]permeability shale and mudstone layers create permeability contrasts that produce artesian conditions locally (Richter, 1981). As with the Quaternary deposits, ground-water heat pumping is the most attractive geothermal potential of the Wind River Formation. It is considerably thicker than the Quaternary deposits, however, and in some areas is overlain by several thousand feet of younger sediments. Thus, relatively high temperatures may be available in deep wells.

Beneath the Wind River Formation, strata begin to develop significant geothermal potential. With greater depth of burial, higher temperatures will occur under normal thermal gradients. The Fort Union - Lance aquifer, for example, is over 10,000 feet deep in the central basin and some reported BHTs exceed $200^{\circ} \mathrm{F}$. The occurrence of major confining units in this section creates artesian conditions in underlying aquifers and the stage is set for the type of forced convection depicted in Figures 3 and 4. Aquifers in the lower Cenozoic and Mesozoic sections are generally dependent on sandstone layers for their productivity. Well yields up to several hundred gallons per minute (gpm) are reported from some of these strata, though most yields fall in the 10 to 50 gpm range. Water quality from these units is quite variable, but is generally poor. Chloride and sulphate are the most common anions; sodium is the dominant cation (Richter, 1981). Since the geothermal potential of the Mesozoic and Paleozoic aquifers is dependent on local structures, generalization beyond overall aquifer productivity and water quality cannot be made.

As the stratigraphic chart indicates (Table 2), there are several major aquifers in the Paleozoic section. Most important of these is the Tensleep Sandstone, which is under significant artesian pressure beneath much of the Wind River Basin. Dana (1962) reported a Tensleep-Madison well near Lander flow-
ing $3,000 \mathrm{gpm}$. Richter (1981) reported that Tensleep wells typically yield up to several thousand gpm. He reported well yields of up to several hundred gpm for the Park City (Phosphoria) and Amsden Formations and the Madison Limestone. Richter proposed that these formations, along with the Darby Formation and the Bighorn Dolomite, be grouped with the Tensleep Sandstone as a single Tensleep aquifer system. This system has generally good-quality water except in the deep, interior basin. Cation dominance varies, but calcium and magnesium are generally greater than sodium. Bicarbonate and sulphate are the dominant anions.

At the base of the sedimentary section is the Flathead Sandstone. This unit has been developed as a highly productive aquifer in parts of the Bighorn Basin. It is known to produce moderate quantities of good-quality water in the Wind River Basin, but has not been significantly developed.

## Structure

The basin is bounded by major mountain uplifts on the north (Owl CreekBridger Mountains), west (Wind River Range), and south (Granite Mountains). These uplifts are complexly folded and faulted areas from which much of the sedimentary rock core has been eroded, leaving Precambrian metamorphic and igneous rocks exposed. Thus, the uplifts form distinct hydrologic as well as structural and topographic boundaries. On the east, the Wind River Basin is bounded by the Casper arch. The oldest exposed rocks along this broad fold are of Jurassic and early Cretaceous age.

Like other Wyoming basins, the Wind River Basin includes many folds and faults superimposed on the overall downwarp of the basin. These structures, along with background heat flow and ground-water circulation patterns, are the principal controls of subsurface temperature distribution.

At sufficient depth, high temperature water could be developed from any of the aquifers discussed above. This is due to the simple increase in temperature with depth that occurs in the earth. In the structurally lowest part of the Wind River Basin, for example, the Flathead Sandstone should contain water hotter than $450^{\circ} \mathrm{F}$. Even so, water temperatures reflecting only normal background gradients are not generally considered valuable enough to justify well drilling costs. A significant geothermal resource will exist only where these deep heated waters are transferred closer to the surface. That transfer can be accomplished artificially with a drill hole or naturally by fold or fault systems such as shown schematically on Figures 3 and 4.

Sheet 3 is a structure contour map of the top of the Early Cretaceous Cloverly Formation. In a general, basin-wide sense, all the sedimentary formations older than Late Cretaceous in the Wind River Basin accumulated as a massive, horizontally layered stack. This stack was deformed during the latest Cretaceous and early Tertiary. Thus, the structural relief depicted for the Cloverly Formation (Sheet 3) is representa-
tive of many higher and lower strata in the basin in all but the absolute elevations.

During and following the period of deformation, sedimentary material was eroded from the uplifts and deposited in the adjacent basin. This created broad, basinward-thickening wedges of the Tertiary sediments. Because these strata, the Fort Union and Wind River Formations, were deposited during and after the deformation of the basin, they are progressively less deformed than underlying strata and less likely to contain thermal gradient anomalies related to fold and fault systems.

Mesozoic and Paleozoic aquifers receive precipitation and runoff recharge where they are exposed at the surface along the basin-bounding uplifts (see Sheet 1). Waters then move basinward, escaping upward where faults or erosion have eliminated confinement. A general circulation pattern for the Cloverly Formation has been proposed by Richter (1981) and is indicated by the arrows on Sheet 3. Because the geometry and recharge patterns of most Mesozoic and Paleozoic strata are similar, flow patterns are assumed to be similar.

## Heat flow

The fundamental component of the geothermal resource is heat flow, the natural flow of thermal energy from the hot interior of the earth to the cool surface. Where heat flow is high, geothermal resources are abundant and less dependent upon other geologic conditions. If heat flow is low, a useful resource is created only where the stratigraphy and structure are favorable.

Heat flow determinations have been made at five sites in the Wind River Basin (Table 3). These values were derived through precision thermal logging and conductivity determinations of holes into Precambrian basement rocks. They are believed to be free of hydrologic
disturbances and representative of regional patterns. The heat flow values come from two general localities: the Granite Mountains along the southern margin of the basin, and the Owl Creek Mountains along the northern margin. Values from the Granite Mountains vary from 50 to $70 \mathrm{~mW} / \mathrm{m}^{2}$. Values from the eastern Owl Creek Mountains indicate a heat flow in the 70 to $80 \mathrm{~mW} / \mathrm{m}^{2}$ range. The northern values are higher than the moderate heat flows of the southern basin. Higher values correspond to a broad zone of moderate to high heat flows that appears to extend across central Wyoming (Sass and Lachenbruch, 1979; Decker and others, 1980). The origin of this zone of higher heat flow

Table 3. Wind River Basin heat flow values. ${ }^{1}$

| Location <br> (Sec-T-R) | Heat flow <br> $\left(\mathrm{mW} / \mathrm{m}^{2}\right)$ | Thermal <br> conductivity <br> $(\mathrm{W} / \mathrm{mOK})$ |
| :--- | :---: | :---: |
| $28-28 \mathrm{~N}-89 \mathrm{~W}$ | 54 | 2.93 |
| $27-28 \mathrm{~N}-92 \mathrm{~W}$ | 60 | 2.93 |
| $27-28 \mathrm{~N}-92 \mathrm{~W}$ | 58 | 2.93 |
| $27-28 \mathrm{~N}-92 \mathrm{~W}$ | 68 | 2.76 |
| $27-28 \mathrm{~N}-92 \mathrm{~W}$ | 74 | 2.76 |
| $27-28 \mathrm{~N}-92 \mathrm{~W}$ | 77 | 2.93 |
| $27-28 \mathrm{~N}-92 \mathrm{~W}$ | 71 | 2.93 |
| $27-28 N-92 \mathrm{~W}$ | 66 | 2.93 |
| $27-28 \mathrm{~N}-92 \mathrm{~W}$ | 64 | 2.93 |
| $6-29 \mathrm{~N}-90 \mathrm{~W}$ | 63 | 3.70 |
| $6-29 \mathrm{~N}-90 \mathrm{~W}$ | 60 | 3.67 |
| $7-30 \mathrm{~N}-90 \mathrm{~W}$ | 50 | 2.34 |
| $18-30 \mathrm{~N}-90 \mathrm{~W}$ | 59 | 2.34 |
| $22-40 \mathrm{~N}-92 \mathrm{~W}$ | 71 | 3.30 |
| $22-40 \mathrm{~N}-92 \mathrm{~W}$ | 79 | 3.30 |

1 Measurements made by University of Wyoming personnel according to procedures described by Decker (1973). Values primarily from Heasler and others (1982).
is not known, and the boundaries are based on rough contouring of the sparse data available. Given the overall structural fabric of the basin, heat flow values are assumed to be most uniform along east-west or northwest-southeast trends. The distribution of the north to south decrease in heat flow cannot be defined without additional, intermediate data points. Analysis of gradient anomalies within the Wind River Basin (see thermal gradient section below) suggests the higher heat flow of the Owl Creek Mountains may extend an unknown distance into the basin.

Breckenridge and Hinckley
(1978) suggested warm springs in the northwestern Wind River Basin may be due to high heat flow associated with the Absaroka volcanic complex. No heat flow determinations have been made for this part of the basin. However, Hinckley and others (1982) calculated that the Absaroka igneous activity is too old to create significant modification of present regional heat flow patterns. The effect on the study area of Late Cenozoic volcanism in the Yellowstone-Teton National Parks area immediately northwest of the Wind River Basin is not clearly understood. This activity is recent enough to create local, presentday heat flow anomalies, but the main centers of activity are distant from the Wind River Basin.

Heat flow determinations in the Wind River Basin indicate geothermal conditions similar to the other Wyoming Basins. In drill holes greater than 4,000 ft deep, purely conductive thermal gradients will generally fall in the $12^{\circ}$ to. $15^{\circ} \mathrm{F} / 1,000$ feet range. Gradients may be slightly higher in the northern basin due to somewhat higher heat flow. Such gradients are not usually considered sufficient to provide a useful geothermal resource by themselves, but will lead to the development of high temperatures at depth. Thus, where ground water warmed at depth is brought close to the surface by circulation over folds or up fault systems, highly elevated gradients and attractive energy resources may exist.

## Areas of anomalous thermal gradients

Information on thermal gradients in the Wind River Basin comes from two sources: oil and gas well bottom-hole temperatures (BHTs), and precision thermal logging. Tables 4 and 5 present summaries of the 1,733 bottom-hole temperatures and calculated gradients collected for the Wind River Basin. Temperatures range from $65^{\circ}$ to $370^{\circ} \mathrm{F}$; gradients range from $2.6^{\circ}$ to $144.4^{\circ} \mathrm{F} / 1,000$ feet. Shallower than approximately 2,500 feet,
all reported temperatures are less than $100^{\circ} \mathrm{F}$ and, along with their calculated gradients, are subject to considerable error as discussed earlier (p.7). Nonetheless, the table lists many gradients greater than $20^{\circ} \mathrm{F} / 1,000$ feet that are confidently based on deep holes with high temperatures. Appendix A lists data from precision thermal logging of wells in the Wind River Basin. These data are plotted on Sheet 2.

Table 4. Summary of bottom-hole temperature data and statistics including the 50 th, 66 th, 80 th, and 90th percentiles, from the Wind River Basin. A temperature under a percentile heading is the temperature below which that percent of the BHTs fall. Depth intervals with few BHT measurements do not give meaningful percentile temperatures.

| Depth interval ( f eet) | Number of measurments | Temperature ( ${ }^{\circ} \mathrm{F}$ ) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | high | Iow | mean | 50\% | 66\% | 80\% | 90\% |
| $0-500$ | 10 | 84 | 65 | 72.4 | 72 | 75 | 82 | 84 |
| $500-1,000$ | 18 | 100 | 60 | 79.2 | 80 | 86 | 94 | 95 |
| 1,000-1,500 | 76 | 152 | 50 | 83.2 | 81 | 90 | 93 | 98 |
| 1,500-2,000 | 103 | 117 | 62 | 88.8 | 89 | 95 | 99 | 103 |
| 2,000-2,500 | 57 | 123 | 62 | 90.7 | 90 | 95 | 97 | 113 |
| 2,500-3,000 | 82 | 146 | 69 | 96.6 | 96 | 102 | 107 | 113 |
| 3,000-3,500 | 164 | 172 | 72 | 107.9 | 109 | 117 | 121 | 126 |
| 3,500-4,000 | 142 | 164 | 79 | 107.8 | 105 | 115 | 121 | 126 |
| 4,000 - 4,500 | 83 | 156 | 78 | 107.1 | 108 | 111 | 117 | 122 |
| 4,500-5,000 | 105 | 171 | 78 | 110.2 | 109 | 113 | 120 | 129 |
| 5,000-5,500 | 92 | 234 | 61 | 117.2 | 116 | 121 | 128 | 131 |
| 5,500-6,000 | 63 | 160 | 89 | 122.1 | 120 | 126 | 138 | 143 |
| 6,000 - 6,500 | 75 | 163 | 97 | 126.9 | 126 | 134 | 143 | 149 |
| 6,500-7,000 | 79 | 185 | 95 | 131.3 | 129 | 135 | 146 | 152 |
| 7,000-7,500 | 75 | 198 | 109 | 142.2 | 138 | 152 | 160 | 180 |
| 7,500-8,000 | 64 | 212 | 64 | 148.9 | 150 | 159 | 164 | 174 |
| 8,000-8,500 | 39 | 182 | 122 | 152.4 | 156 | 162 | 168 | 175 |
| 8,500-9,000 | 46 | 190 | 112 | 150.7 | 151 | 160 | 166 | 181 |
| 9,000-9,500 | 27 | 195 | 120 | 153.2 | 151 | 165 | 171 | 184 |
| 9,500-10,000 | 34 | 230 | 68 | 158.3 | 160 | 169 | 180 | 205 |
| 10,000-10,500 | 34 | 250 | 125 | 175.0 | 181 | 189 | 204 | 215 |
| 10,500-11,000 | 31 | 214 | 124 | 163.8 | 163 | 173 | 184 | 198 |
| 11,000-11,500 | 45 | 240 | 134 | 187.4 | 192 | 199 | 205 | 211 |
| 11,500-12,000 | 43 | 250 | 142 | 196.9 | 195 | 202 | 208 | 214 |
| 12,000-12,500 | 22 | 260 | 135 | 197.0 | 208 | 214 | 217 | 225 |
| 12,500-13,000 | 14 | 306 | 170 | 217.9 | 212 | 226 | 242 | 265 |
| 13,000-13,500 | 12 | 245 | 159 | 207.2 | 216 | 238 | 238 | 240 |
| 13,500-14,000 | 17 | 267 | 172 | 221.2 | 230 | 240 | 255 | 264 |
| 14,000-14,500 | 9 | 268 | 218 | 245.7 | 256 | 262 | 262 | 268 |
| 14,500-15,000 | 6 | 290 | 174 | 246.8 | 268 | 281 | 281 | 290 |
| 15,000-15,500 | 7 | 284 | 200 | 241.4 | 250 | 252 | 265 | 284 |
| 15,500-16,000 | 7 | 292 | 216 | 248.3 | 252 | 254 | 270 | 292 |
| 16,000-16,500 | 11 | 316 | 245 | 294.0 | 305 | 309 | 314 | 316 |
| 16,500-17,000 | 2 | 278 | 258 | 268.0 | 278 | 278 | 278 | 278 |
| 17,000-17,500 | 4 | 340 | 317 | 331.3 | 338 | 338 | 340 | 340 |
| 17,500-18,000 | 8 | 345 | 268 | 315.3 | 338 | 340 | 345 | 345 |
| 18,000-18,500 | 9 | 345 | 308 | 331.2 | 337 | 338 | 344 | 345 |
| 18,500-19,000 | 2 | 351 | 338 | 344.5 | 351 | 351 | 351 | 351 |
| 19,000-19,500 | 5 | 356 | 318 | 331.4 | 325 | 340 | 356 | 356 |
| 19,500-20,000 | 4 | 343 | 318 | 327.3 | 343 | 343 | 343 | 343 |
| 20,000-20,500 | 1 | 310 | 310 | 310.0 | 310 | 310 | 310 | 310 |
| 20,500-21,000 | 3 | 348 | 323 | 338.0 | 343 | 348 | 348 | 348 |
| 21,000-21,500 |  |  |  |  | - | - | - | - |
| 21,500-22,000 | 2 | 370 | 309 | 339.5 | 370 | 370 | 370 | 370 |
| 22,000-22,500 |  |  |  |  | - | - | - | - |
| 22,500-23,000 | 1 | 370 | 370 | 370.0 | 370 | 370 | 370 | 370 |

Total: 1,733 bottom-hole temperature measurements.

Table 5. Summary of thermal gradient data and statistics, including the $50 \mathrm{th}, 66 \mathrm{th}, 80 \mathrm{th}$, and 90 th percentiles, derived from the bottom-hole temperatures from the Wind River Basin. A gradient under a percentile heading is the gradient below which that percent of the gradients fall. Depth intervals with few BHT measurements do not give meaningful percentile temperatures.

| Depth Interval ( f eet) | Numberofmeasurements | Gradient ( ${ }^{\circ} \mathrm{F} / 1,000 \dagger t$ ) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | high | Iow | mean | 50\% | 66\% | 80\% | 90\% |
| 0-500 | 10 | 144 | 48 | 79.0 | 67 | 72 | 104 | 144 |
| 500-1,000 | 18 | 81 | 20 | 45.9 | 45 | 50 | 55 | 65 |
| 1,000-1,500 | 76 | 77 | 5 | 30.9 | 30 | 34 | 39 | 43 |
| 1,500-2,000 | 103 | 43 | 11 | 26.4 | 25 | 28 | 31 | 34 |
| 2,000-2,500 | 57 | 37 | 9 | 21.4 | 21 | 23 | 24 | 29 |
| 2,500-3,000 | 82 | 39 | 8 | 19.5 | 19 | 21 | 22 | 24 |
| 3,000-3,500 | 164 | 38 | 8 | 19.6 | 19 | 21 | 23 | 24 |
| 3,500-4,000 | 142 | 30 | 9 | 17.5 | 16 | 19 | 21 | 22 |
| 4,000-4,500 | 83 | 26 | 8 | 15.2 | 14 | 15 | 17 | 18 |
| 4,500-5,000 | 105 | 26 | 7 | 14.1 | 13 | 14 | 16 | 18 |
| 5,000-5,500 | 92 | 35 | 3 | 14.1 | 13 | 14 | 15 | 17 |
| 5,500-6,000 | 63 | 20 | 7 | 13.8 | 13 | 14 | 16 | 17 |
| 6,000-6,500 | 75 | 18 | 8 | 13.4 | 13 | 14 | 15 | 16 |
| 6,500-7,000 | 79 | 20 | 7 | 13.0 | 12 | 13 | 15 | 16 |
| 7,000-7,500 | 75 | 21 | 9 | 13.7 | 12 | 15 | 16 | 18 |
| 7,500-8,000 | 64 | 21 | 2 | 13.6 | 13 | 14 | 15 | 17 |
| 8,000-8,500 | 39 | 17 | 9 | 13.3 | 13 | 14 | 15 | 15 |
| 8,500-9,000 | 46 | 16 | 7 | 12.3 | 12 | 13 | 13 | 15 |
| 9,000-9,500 | 27 | 16 | 8 | 11.9 | 11 | 13 | 13 | 15 |
| 9,500-10,000 | 34 | 19 | 2 | 11.8 | 11 | 12 | 13 | 16 |
| 10,000-10,500 | 35 | 20 | 7 | 12.9 | 12 | 14 | 15 | 16 |
| 10,500-11,000 | 31 | 16 | 7 | 11.3 | 11 | 12 | 12 | 14 |
| 11,000-11,500 | 46 | 17 | 8 | 12.8 | 13 | 13 | 14 | 14 |
| 11,500-12,000 | 43 | 17 | 8 | 13.1 | 12 | 13 | 14 | 14 |
| 12,000-12,500 | 24 | 17 | 7 | 12.7 | 13 | 13 | 14 | 14 |
| 12,500-13,000 | 13 | 17 | 9 | 13.2 | 13 | 13 | 14 | 15 |
| 13,000-13,500 | 12 | 15 | 8 | 12.3 | 12 | 13 | 14 | 14 |
| 13,500-14,000 | 19 | 16 | 9 | 12.8 | 12 | 14 | 14 | 15 |
| 14,000-14,500 | 9 | 15 | 12 | 14.3 | 15 | 15 | 15 | 15 |
| 14,500-15,000 | 6 | 16 | 8 | 13.8 | 15 | 16 | 16 | 16 |
| 15,000-15,500 | 6 | 15 | 10 | 13 | 13 | 14 | 14 | 15 |
| 15,500-16,000 | 7 | 15 | 10 | 13.1 | 13 | 13 | 14 | 15 |
| 16,000-16,500 | 12 | 16 | 10 | 15.0 | 16 | 16 | 16 | 16 |
| 16,500-17,000 | 2 | 14 | 12 | 13.5 | 14 | 14 | 14 | 14 |
| 17,000-17,500 | 4 | 17 | 15 | 16.7 | 17 | 17 | 17 | 17 |
| 17,500-18,000 | 9 | 17 | 12 | 15.3 | 16 | 16 | 16 | 17 |
| 18,000-18,500 | 9 | 16 | 14 | 15.8 | 15 | 16 | 16 | 16 |
| 18,500-19,000 | 2 | 16 | 15 | 16.2 | 16 | 16 | 16 | 16 |
| 19,000-19,500 | 5 | 16 | 14 | 15.0 | 14 | 15 | 16 | 16 |
| 19,500-20,000 | 4 | 15 | 13 | 14.3 | 14 | 14 | 15 | 15 |
| 20,000-20,500 | 1 | 13 | 13 | 13.1 | 13 | 13 | 13 | 13 |
| 20,500-21,000 | 3 | 14 | 13 | 14.3 | 14 | 14 | 14 | 14 |
| 21,000-21,500 | - | - | - | - | - | - | - | - |
| 21,500-22,000 | 2 | 15 | 12 | 13.7 | 15 | 15 | 15 | 15 |
| 22,000-22,500 | - | - | - | - | - | - | - | - |
| 22,500-23,000 | 1 | 14 | 14 | 14.5 | 14 | 14 | 14 | 14 |

Gradient $=\frac{$\begin{tabular}{c}
Bottom-hole <br>
temperature

$-$

Mean annual surface <br>
temperature
\end{tabular}}{Depth}$\times 1,000$

An alternative view of the BHT data is presented in Figure 6, which shows the effect of drilling mud in creating unrealistically high gradients at shallow depths. The divergence of the $100^{\circ} \mathrm{F}$ mud curve from a significant portion of the data (for example the $80 t h$ percentile curve) indicates that only below 2,000 to 3,000 feet will thermal gradients be consistently free of drill-ing-fluid induced increases. Points to the right of the 80 th percentile line on this plot are those considered to represent possibly significant geothermal anomalies.

Figure 7 plots bottom-hole temperatures by depth. Reference lines for gradients of $12^{\circ}$ and $14^{\circ} \mathrm{F} / 1,000$ feet are included. Note the general agreement of these data with the $12^{\circ}$ to $15^{\circ} \mathrm{F} / 1,000$ feet average gradient proposed earlier on the basis of heat flow and thermal conductivity considerations.

The areal distribution of gradients is presented on Sheet 2. All available bottom-hole temperature, thermal logging, thermal spring, thermal well, and heat flow data are plotted on this map and approximate gradient contours are proposed. Where gradients identified as anomalous (based on Table 5 and Figure 6) occur in the same vicinity, an area of anomalous gradient is mapped. Due to the uncertainty of individual gradient points, contours and anomalous areas are generally based on consideration of a group of values for a given area.

Table 6 provides summary information on each of the areas of anomalous gradient identified on Sheet 2. The thermal gradients in Table 6 are calculated from depths and temperatures for the listed principal formations. While there is no implication that the anomaly is confined to these brackets, extrapolation to much shallower or much deeper zones must be done cautiously.

Even in these anomalous areas, gradients are not extreme. Nowhere, for ex-
ample, are there confirmed gradients as high as those for the Thermopolis and Cody areas of the Bighorn Basin (Heasler and Hinckley, 1985). Since the estimated heat flow into the Wind River Basin is generally insufficient to create conductive gradients higher than $12^{\circ}$ to $15^{\circ} \mathrm{F} / 1,000$ feet, geothermal anomalies are primarily a function of convective redistribution of heat. The complex interaction of ground water and geologic structure is the principle geothermal agent. The following pages discuss what is known or can be deduced about that interaction in the Wind River Basin. General principles are developed, along with individual system specifics, through analysis of each of the mapped anomalous areas. Considerations of temperatures, depths, and general character of the potential geothermal resource, and possible, unverified extensions of the anomalous areas are included. The density of data points on Sheet 2 demonstrates the variation in certainty with which anomalous areas are identified. In many cases, additional thermal logging, geochemical studies, and (or) structural analysis would be useful in verifying the indicated anomaly.

## Area 1

Area 1 essentially coincides with the Dubois oil field. The structure is complicated and not well understood in this area. The thick mantle of volcanic rocks in the area further confuses outcrop/ recharge relationships. The anomaly is well defined by numerous data points of sufficient depth and temperature to be free of the most obvious sources of error. Hydrologic control is assumed to be some combination of folding and faulting of undetermined extent.

## Areas 2 and 3

The high gradients of area 2 are among the best established of any in the Wind River Basin. In addition to abundant oil and gas well bottom-hole


Figure 6. Gradient-depth plot for Wind River Basin, based on 1,733 bottom-hole temperatures.


Figure 7. Bottom-hole-temperature depth plot for Wind River Basin, based on 1,733 bottom-hole temperatures.

Table 6. Geothermal gradient anomalies in the Wind River Basin, Wyoming.

temperature data, there are a confirming thermally logged hole and a major hot spring (see Sheet 2). Sheet 3 shows the intersection of the area with a major fault system paralleling nearly the entire length of the Wind River Range. In addition, at area 2 there is a significant fold immediately northeast of the fault system. The indicated ground-water flow direction is northeastward and eastward off the flank of the mountains, descending into the Wind River Basin. Subtracting the structure contour elevations ( $0-1,000$ feet) from the approximate surface elevation (6,000 feet) shows the top of the Cloverly to be around 6,000 feet deep adjacent to the fault. Addition of the intervening strata (see Table 2) places the Phosphoria Formation at 8,500 feet with the Madison Limestone at 9,500 feet. A gradient of only $12^{\circ} \mathrm{F} / 1,000$ feet would thus lead to ground-water temperatures of about $150^{\circ} \mathrm{F}$ in the Madison Limestone. Displacements across the fault system range from 3,000 to 6,000 feet. In the
vicinity of area 2 , strata are uplifted approximately 4,000 feet on the northeast side of the fault. Folding has raised the strata an additional 3,000 feet (see Sheet 2). Waters in the Paleozoic aquifers remain confined beneath relatively impermeable strata, moving up and over the fault/fold system and delivering deep-heated waters to the near surface.

The presence of the Paleozoic aquifers at relatively shallow depths is particularly advantageous in this area due to their productivity and their relatively high water quality. The depth/gradient calculations for this system indicate around $140^{\circ} \mathrm{F}$ as the maximum temperature likely to be encountered. This is in reasonable agreement with the $100^{\circ}$ to $130^{\circ} \mathrm{F}$ bottom-hole temperatures reported when allowances are made for moving ground water cooling the deep portion of the system and for some cooling as waters ascend to shallower zones.

Area 3 is basically a less anomalous version of area 2. The synclinal portion of the system is shallower; the anticlinal portion is deeper; and the gradient anomaly is correspondingly weaker than in area 2. The flow system appears to be quite similar.

The major complication in the flow systems of areas 2 and 3 is faulting。 Where strata are simply deformed into folds, stratigraphic continuity and ground-water flow patterns are generally maintained (although the fracturing attending folding of competent rock layers may greatly enhance permeabilities). The effect of faulting, however, is quite variable. Faulting may create ground-water pathways through normally confining beds, allowing deep-heated waters to rise to the near surface and creating thermal gradient anomalies in the absence of folding. On the other hand, faulting may produce tight, impermeable zones that seriously restrict ground-water movement. Also, the juxtaposition of permeable and impermeable strata across a fault may reduce or eliminate hydraulic continuity. Because the configuration of a fault may be spatially quite variable, the effect of the fault on hydrologic systems can be locally unpredictable. In addition, large deep faults presented on Sheet 3 are somewhat conjectural, based on interpretation of subsurface data, in some cases with little or no surface expression.

The effect of large-scale faulting on geothermal systems can best be analyzed empirically. The existence of geothermal anomalies strongly suggests that water is moving up and across the fault system in the vicinity of areas 2 and 3 . Elsewhere along the fault the effect is different. North of area 2, for example, there are many bottom-hole temperature data points, yet no gradient anomaly is indicated. The deep syncline just west of the fault and the 5,000-foot fault displacement could provide the setting for a major thermal gradient anomaly. But apparently the fault in this area does not permit the free passage of
ground water. Such restriction is also indicated by ground-water flow parallel to the fault system in this area as proposed by Richter (1981) (see Sheet 2).

There are few data points to confirm or deny a gradient anomaly between areas 2 and 3. If the general ground-water flow directions of Richter (1981) are correct, the anomaly may extend all along the length of the fault (although adjacent folding is most developed in and around areas 2 and 3 ). The thermal well southeast of Lander is also on this fault system. It flows $99^{\circ} \mathrm{F}$ water from a depth of 1,884 feet for a gradient of $30^{\circ} \mathrm{F} / 1,000$ feet. Bottom-hole temperature values between here and area 3 do not indicate high gradients, but data are sparse. Thus, it is not known whether the Lander well marks an isolated area of anomalous gradient or a continuation of the area 3 anomaly along the fault.

## Area 4

Area 4 is established by only 2 data points, both from depths of approximately 3,000 feet. The area occupies the crest of a major fold where it could receive a component of ground-water flow from deep areas to the southwest.

## Area 5

Area 5 is established by three data points. These points range over 6,500 feet of depth. The fairly high temperatures from this area are unlikely to have been increased by surface conditions. The area is located near the top of a fold, the southeast limb of which is faulted as it dips steeply into the adjacent syncline. Confined ground water arriving at area 5 from the east and southeast rises around 7,000 feet in four miles. For the Cloverly Formation, this is sufficient to produce a gradient of $25^{\circ} \mathrm{F} / 1,000$ feet and temperatures of over $200^{\circ} \mathrm{F}$ (based on a background gradient of $12^{\circ} \mathrm{F} / 1,000$ feet). For the Tensleep Sandstone, approximately 2,500 feet deeper, around $30^{\circ} \mathrm{F}$ can be added.

Ground-water flow from the southwest could produce only normal gradients at area 5 and is therefore not indicated. Also, it appears that the fault just west of area 5 does not seriously restrict ground-water movement.

## Area 6

Area 6 is in essentially the same configuration as area 5, except that area 6 occupies both sides of the fault. This is additional evidence that the fault is not a ground-water barrier and that it may actually create a fractured zone of locally increased permeability. Gradients are somewhat lower in area 6 than in area 5, reflecting the shallower nature of the adjacent syncline. This anomaly may extend all along the fault/ fold system between areas 6 and 5. However, numerous data northwest of area 5 indicate a generally normal gradient in that area.

## Area 7

Area 7 coincides with the faulted portion of the Conant Creek anticline. Thermal springs issue from the Phosphoria Formation in this area, where erosion has cut through the confining beds of the Chugwater Formation near the anticlinal crest. Although the springs flow only $61^{\circ} \mathrm{F}$, within a third of a mile is a well (with more direct subsurface access) flowing $70^{\circ} \mathrm{F}$ (Breckenridge and Hinckley, 1978). The Phosphoria and Tensleep aquifers plunge northward from the spring site, and bottom-hole temperatures are as high as $140^{\circ} \mathrm{F}$ from 4,000 to 5,000 feet deep. Breckenridge and Hinckley (1978) discussed this geothermal system in reference to the springs and presented the model of northeastward ground-water flow heated in the depths of the syncline between area 7 and area 8. Any flow from the west or southwest would be adequate to produce the observed temperatures in the Paleozoic
formations at area 7. Richter's (1981) proposal of flow from the southeast would almost certainly be inadequate, and is therefore not indicated.

## Area 8

Area 8 is defined by numerous and consistent bottom-hole temperatures from deep zones with high temperatures. Although there are no surface flows from this system, thermal logging confirms the bottom-hole temperature derived gradients. Most of the temperature values are from $150^{\circ}$ to $180^{\circ} \mathrm{F}$ and come from the Tensleep Sandstone. The highest temperature reported for this area is $234^{\circ} \mathrm{F}$ from the Phosphoria Formation at a depth of 5,443 feet. Like most of the anomalous areas discussed so far, area 8 occupies the top of a fold, adjacent to a fault with large displacement ( 2,000 to 3,000 feet) and a deep syncline. The Tensleep Sandstone is approximately 12,000 feet deep just west of area 8 , and is around 10,000 feet deep even in the shallower part of the syncline south of the anomaly. This is sufficient to produce temperatures of $180^{\circ} \mathrm{F}$ even at a $12^{\circ} \mathrm{F} / 1,000$ feet gradient. Ground-water flow from the structural depression just northwest of area 8 would be $230^{\circ} \mathrm{F}$ at this gradient. Thus, the gradient anomaly is consistent with ground-water flow northward and eastward off the flanks of the Wind River Range, through the intervening syncline, and up the fold/fault system to area 8.

As in previous cases, this interpretation of the anomaly requires that the fault not seriously impede ground-water movement in the vicinity. Bottom-hole temperatures north and south of area 8 along the same structural trend are not generally anomalous. Changes in the hydrologic effect of the fault or hydraulic conductivity of the aquifer are possible explanations for this gradient distribution.

## Areas 9, 10, and 11

Areas 9, 10, and 11 are weak anomalies. Gradients of $15^{\circ}$ to $20^{\circ} \mathrm{F} / 1,000$ feet are well established by deep wells into a variety of upper Mesozoic and lower Cenozoic strata. The highest reported temperature in these areas is $348^{\circ} \mathrm{F}$, from a depth of 20,853 feet in area 9. These areas occupy one of the structurally lowest portions of the Wind River Basin, just south of a major and complex fault zone. The Precambriancored Owl Creek-Bridger Mountains are on the uplifted north side of this fault system. Displacements of more than 20,000 feet are common; stratigraphic and hydrologic disruption is total. Due to the great depths involved and the very thick Tertiary section in this area, pre-Cenozoic structure is not well known. As discussed earlier, Sheet 3 is compiled for the Cloverly Formation but corresponds in general geometry to all strata deposited prior to the folding and faulting of the Cloverly Formation. The rocks of areas 9,10 , and 11 were deposited during and following these deformational events, which further complicates understanding of the structural environment of any geothermal systems.

Area 9 roughly conforms to the crest of a broad anticline, as defined by the Cloverly Formation contouring of Sheet 3. Structural mapping by Barlow and Haun (1978) indicated this fold involves strata as young as the Waltman Shale Member of the Fort Union Formation. Ground-water flow is not known for the area, so maximum temperatures and the extent of the the anomaly cannot be predicted. Because of the great thickness of the overlying Wind River Formation, and the moderate gradients involved, this anomaly probably only represents a useful resource where existing drilling provides subsurface access.

The origin of areas 10 and 11 is even less clear, for no folds or faults are indicated. There may be unrecognized structures controlling the flow of
heated ground water in these deep systems. Given the total thickness of sedimentary rocks in these areas, temperatures in excess of $400^{\circ} \mathrm{F}$ may be generated in the Paleozoic aquifers under normal gradients. If the ground water in these units flows into higher strata, significant gradient anomalies could exist.

An alternative explanation for the apparent anomalies in areas 9 through 11 is higher heat flow. Measured heat flows to the north, in the Owl Creek Mountains, are sufficient to create purely conductive gradients in the range of those observed (depending on formation thermal conductivities). If these higher heat flows extend into the basin beneath areas 9 through 11 , the moderately high gradients observed could be explained without convective heat transport.

## Area 12

Area 12 is on the margin of the Wind River Basin, in a structural setting similar to that of areas 6 through 8 。 The area occupies the crest of a northtrending anticline; there are also major faults through the area. The elevation difference between the anticline crest and adjacent synclinal areas is insufficient to create the observed anomaly. Thus, vertical migration of ground water along the faults is a more likely gradient-increasing mechanism. The thermal gradients of the three data points identifying area 12 are not high, however, and more data are needed to verify these gradients.

## Area 13

Area 13 is in a complexly faulted region that is an extension of the basin-bounding fault system of area 9 . In this structural environment it is highly unlikely that continuous confined aquifers exist. It is much more difficult to assess the geothermal effects of fault-created zones of vertical permeability than to analyze
simple fold systems. At the present, we can only infer that waters heated in deeper strata are rising along fault zones to create the gradient anomalies observed in overlying units. If so the anomaly will decrease with depth.

## Area 14

Area 14 appears to be fold control-
led. Waters confined to the Tensleep aquifer and moving into the area from the south and southeast pass through depths sufficient to produce the observed temperatures $\left(120^{\circ}\right.$ to $\left.170^{\circ} \mathrm{F}\right)$ under normal thermal gradients. Waters in deeper aquifers may be $20^{\circ}$ to $30^{\circ} \mathrm{F}$ warmer, so the maximum temperature likely to be developed for this area is less than $200^{\circ} \mathrm{F}$.

## Thermal springs

Breckenridge and Hinckley (1978) identified seven thermal spring localities in the Wind River Basin. They provided detailed discussions of water temperatures, flows, chemistry, and flora. Fort Washakie Hot Springs and Conant Creek Springs were discussed above in connection with anomalous gradient areas 2 and 7, respectively. Although the remaining five localities are definitely geothermally anomalous, they were not included in the previous discussion, which was based primarily on subsurface thermal information. All seven thermal spring localities are shown on Sheet 2.

Horse Creek Springs are in the southeast corner of the basin (sec. 35,
 ridge and Hinckley (1978) the springs flow at $75^{\circ} \mathrm{F}$ from alluvium along the east-west-trending north Granite Mountains fault system. Eocene igneous rocks in the area and deep circulation along the fault system are offered as possible heating mechanisms. As discussed earlier, igneous activity of this age is probably too old to continue to contribute significant heat. The fault system is the most plausible mechanism for the thermal springs, raising the possibility that a thermal anomaly may extend for some distance east and west from the springs.

Sweetwater Station Springs (sec. 15, T. $29 \mathrm{~N} ., \mathrm{R} .95 \mathrm{~W}$.), west of Jeffrey City, are also fault controlled (Breckenridge and Hinckley, 1978). Nearby bottom-hole
temperatures reflect normal gradients, indicating that the spring system is localized.

The most enigmatic geothermal phenomena in the basin are the thermal springs near Dubois. From north to south these three spring localities are: Warm Spring Creek Springs (sec. 32, T.42N., R. 107W.), Little Warm Spring (sec. 14, T.41N., R. 107W.) , and Jakeys Fork Spring (sec. 29, T.41N., R.106W.). Together, they flow a total of 700 gpm at an average temperature of $78^{\circ} \mathrm{F}$ (Breckenridge and Hinckley, 1978). These springs define a line parallel to the northeast flank of the Wind River Range (Sheet 2). All three localities are along the contact of the Phosphoria Formation and the overlying Chugwater Formation. Extensive travertine deposits, developed southeast from the springs over 30 miles, reflect this same strong stratigraphic control (Breckenridge and Hinckley, 1978). Gilliland (1959) reported a total sub-Chugwater sedimentary thickness of 3,000 feet. Mapping by both Gilliland (1959) and Keefer (1970) indicated no significant disruption of the gentle basinward dip of the strata in this area, and nearby bottom-hole temperatures indicate gradients no higher than $15^{\circ} \mathrm{F} / 1,000$ feet. Thus, circulation of ground water to the lowest strata in the sedimentary section is necessary to produce the observed temperatures at the indicated gradient, yet there is no sign that such a circulation system exists.

## Tensleep aquifer temperatures

The usefulness of geothermal energy in a particular area is governed by two main parameters: (1) the geothermal gradient (which indicates how deep one must drill to encounter the desired temperature) and (2) the availability of a mechanism for extracting the heat from the earth. The chemistry of geothermal waters can also be important, depending on the intended application. At the relatively low temperature of Wind River Basin geothermal resources, naturally occurring circulation of ground water is necessary both to create gradient anomalies (as discussed above) and to provide a mechanism for heat extraction. Only where a productive aquifer occurs can a useful geothermal resource exist.

The Tensleep Sandstone was chosen to present the temperatures occurring in the aquifers of the Wind River Basin (Sheet 4). This sandstone is a major aquifer basinwide and is also one of the deeper aquifers. It is approximately 2,000 feet from the Tensleep Sandstone to the base of the sedimentary section
(the maximum depth of any possible aquifer system). Thus, maximum groundwater temperatures in even the Flathead aquifer will not be more than $20^{\circ}$ to $30^{\circ} \mathrm{F}$ warmer than those of the Tensleep Sandstone. Where an anomaly exists due to vertical, interformational flow along a fault or fracture zone, temperatures may be homogeneous through the strata involved and interformational thermal gradients may drop to near zero.

Sheet 4 was compiled using only temperatures that could be identified as being from the Tensleep Sandstone. In areas of sparse data, the structure contour map (Sheet 3) was used to guide contouring. In the north-central areas of the Wind River Basin, the depth of the Tensleep Sandstone is greater than 20,000 feet. Data from such great depths are sparse. Our estimation of temperatures greater than $400^{\circ} \mathrm{F}$ is based on the extrapolation of high temperatures measured in the much shallower Fort Union Formation.

## Summary and conclusions

Background heat flow in the Wind River Basin is generally insufficient to produce high conductive gradients. High temperatures will occur at shallow depths only where hydrologic systems redistribute heat through water movement. Aquifers that may have the confinement and structural characteristics necessary to create such geothermal systems are the Lance-Fort Union, Mesaverde, Frontier, Muddy, Cloverly, Sundance, Nugget, Phosphoria, Tensleep, Amsden, Madison, Bighorn, and Flathead formations. Of these, the Tensleep Sandstone and Madison Limestone are the most attractive in terms of both productivity and water quality.

Folds and faults provide structural control on hydrology (and hence geothermal systems). Oil and gas exploration
holes are common in folded regions, and generally provide sufficient temperature data to evaluate geothermal gradients. Where faulting alone provides the flow patterns necessary to generate a geothermal anomaly, high gradients may be localized, drilling may be less common, and the data used in this report may be insufficient to delineate such an anomaly. Fault systems tentatively identified as anomalous by bottom-hole temperatures and(or) the occurrence of thermal springs warrant further study.

Most of the identified geothermal anomalies in the Wind River Basin occur along complex structures in the southwest and south. Large, weakly anomalous areas in the north-central basin area are unexplained and may simply reflect the overall increase in heat flow be-
lieved to occur from south to north across the basin.

The most attractive geothermal prospects identified are anomalous areas 2 and 3 north of Lander, Sweetwater Station Springs west of Jeffrey City, and the thermal springs southwest of Dubois. Even in these areas, it is unlikely that aquifer temperatures are higher than $130^{\circ}$ to $150^{\circ} \mathrm{F}$. Geothermal resources elsewhere in the study area are probably best pursued in conjunction with oil and gas production or water-development projects. Particularly in the Paleozoic aquifers, the coincidence of structurally controlled oil and gas deposits and useful thermal waters is very likely. This may allow exploitation of more valuable petroleum resources to pay drilling and development costs, with thermal waters being produced as a valuable by-product.

There is also potential in the Wind River Basin for normal-temperature geothermal applications such as groundwater heat pumps and surface deicing operations. The extensive surface occurrence of the highly productive Wind River Formation is very favorable in this respect, for small supplies of $40^{\circ}$ to $50^{\circ} \mathrm{F}$ ground water should be readily available over a large portion of the basin.

Areas in which further studies of geothermal potential could be most useful are the fault systems previously mentioned and the thermal springs system in the vicinity of Dubois. Not only would such studies help to define potentially significant energy resources, but they may also provide useful data on overall basin hydrogeology.

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Appendix A

Appendix A. Thermally measured wells in the Wind River Basin.

| Location |  |  |  | Depth |  | Bottom-hole Temperature ( ${ }^{\circ} \mathrm{C}$ ) ( ${ }^{\circ} \mathrm{F}$ ) |  | Gradient ${ }^{2}$ |  | Interval ${ }^{3}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Longi | tude |  | Itude | Meters | Feet |  |  | ${ }^{\circ} \mathrm{C} / \mathrm{km}{ }^{\circ} \mathrm{F}$ | 000 ft | Meters | Feet |
| Fremont County |  |  |  |  |  |  |  |  |  |  |  |
| $109{ }^{\circ}$ | 42.11 | $43^{\circ}$ | 38.51 | 67.9 | 223 | 6.6 | 43.8 | 10.0 | 5.5 | 131- 220 | 400- 670 |
| $109{ }^{\circ}$ | 38.51 | $43^{\circ}$ | 37.21 | 630.0 | 2,066 | 25.7 | 78.3 | 31.1 | 17.1 | 295- 688 | 900-2,100 |
| $109{ }^{\circ}$ | 2.31 | $43^{\circ}$ | 31.4' | 274.0 | 899 | 16.0 | 60.8 | 29.3 | 16.1 | 66-899 | 200-2,740 |
| $109{ }^{\circ}$ | 2.21 | $43^{\circ}$ | 31.31 | 284.5 | 933 | 18.1 | 64.5 | 25.8 | 14.1 | 558-787 | 1,700-2,400 |
| $109{ }^{\circ}$ | 2.41 | $43^{\circ}$ | 31.11 | 208.5 | 684 | 13.8 | 56.8 | 25.4 | 13.9 | 328-682 | 1,000-2,080 |
| $107^{\circ}$ | 54.51 | $43^{\circ}$ | 24.71 | 193.5 | 635 | 13.6 | 56.4 | 23.5 | 12.9 | 66- 633 | 200- 1,930 |
| $107{ }^{\circ}$ | 54.8' | $43^{\circ}$ | 24.61 | 193.0 | 633 | 13.4 | 56.1 | 21.3 | 11.7 | 328- 633 | 1,000-1,930 |
| $107^{\circ}$ | $54.5{ }^{\prime}$ | $43^{\circ}$ | 24.51 | 197.5 | 648 | 13.4 | 56.1 | 23.0 | 12.6 | 361-623 | 1,100-1,900 |
| $107^{\circ}$ | 52.61 | $43^{\circ}$ | 24.51 | 172.2 | 565 | 12.5 | 54.5 |  |  |  |  |
| $107^{\circ}$ | 55.01 | $43^{\circ}$ | $24.4{ }^{1}$ | 140.7 | 461 | 11.9 | 53.4 | 20.2 | 11.1 | 328-459 | 1,000-1,400 |
| $107^{\circ}$ | 55.01 | $43^{\circ}$ | $24.4{ }^{1}$ | 141.0 | 462 | 11.9 | 53.4 | 20.2 | 11.1 | 328-459 | 1,000-1,400 |
| $107^{\circ}$ | 54.8' | $43^{\circ}$ | 24.41 | 190.7 | 625 | 13.7 | 56.6 | 19.7 | 10.8 | 262- 623 | 800- 1,900 |
| $107{ }^{\circ}$ | 53.51 | $43^{\circ}$ | $24.4{ }^{1}$ | 133.2 | 437 | 10.7 | 51.2 | 4.2 | 2.3 | 30- 436 | 90- 1,330 |
| $107^{\circ}$ | 52.91 | $43^{\circ}$ | 24.41 | 152.0 | 499 | 13.3 | 55.9 | 34.4 | 18.9 | 66-492 | 200- 1,500 |
| $107^{\circ}$ | 51.71 | $43^{\circ}$ | $24.4{ }^{1}$ | 99.5 | 326 | 11.0 | 51.8 | 24.3 | 13.3 | 164-325 | 500- 990 |
| $107^{\circ}$ | $52.5{ }^{\prime}$ | $43^{\circ}$ | 24.31 | 164.3 | 539 | 12.6 | 54.6 | 5.3 | 2.9 | 95- 538 | 290- 1,640 |
| $107^{\circ}$ | 53.41 | $43^{\circ}$ | 24.21 | 118.7 | 389 | 11.6 | 52.8 | 6.8 | 3.7 | 98- 387 | 300-1,180 |
| $107^{\circ}$ | 53.71 | $43^{\circ}$ | 24.11 | 84.3 | 309 | 12.2 | 54.0 | 6.3 | 3.5 | 30- 276 | 90- 840 |
| $107^{\circ}$ | 51.21 | $43^{\circ}$ | 20.71 | 40.0 | 131 | 13.1 | 55.6 |  |  |  |  |
| $107^{\circ}$ | $51.4{ }^{\prime}$ | $43^{\circ}$ | 20.61 | 75.0 | 246 | 12.6 | 54.6 |  |  |  |  |
| $107^{\circ}$ | 51.41 | $43^{\circ}$ | 20.61 | 89.0 | 292 | 11.4 | 52.5 | 20.0 | 11.0 | 197-292 | 600- 890 |
| $107^{\circ}$ | 52.01 | $43^{\circ}$ | 20.31 | 173.0 | 567 | 15.3 | 59.5 |  |  |  |  |
| $108^{\circ}$ | 54.21 | $43^{\circ}$ | 16.31 | 1,610.0 | 5,281 | 53.5 | 128.3 | 30.2 | 16.6 | 656-5,281 | 2,000-16,100 |
| $108^{\circ}$ | 53.61 | $43^{\circ}$ | 7.01 | 165.0 | 541 | 17.0 | 62.6 | 60.1 | 33.0 | 262- 535 | 800-1630 |
| $108^{\circ}$ | 53.41 | $43^{\circ}$ | 7.01 | 1,080.0 | 3,542 | 53.3 | 127.9 | 36.3 | 20.0 | 1,115-3,542 | 3,400-16,100 |
| $107^{\circ}$ | 35.51 | $42^{\circ}$ | 54.71 | 38.0 | 125 | 9.5 | 49.1 |  |  |  |  |
| $107^{\circ}$ | 32.91 | $42^{\circ}$ | 54.61 | 38.0 | 125 | 7.2 | 44.9 |  |  |  |  |
| $107^{\circ}$ | 32.71 | $42^{\circ}$ | 54.61 | 66.0 | 216 | 9.5 | 49.1 |  |  |  |  |
| $107^{\circ}$ | 32.31 | $42^{\circ}$ | 54.61 | 58.0 | 190 | 9.4 | 49.0 |  |  |  |  |
| $107^{\circ}$ | 31.11 | $42^{\circ}$ | 54.61 | 63.0 | 207 | 9.9 | 49.8 |  |  |  |  |
| $107^{\circ}$ | 33.21 | $42^{\circ}$ | 54.41 | 52.0 | 171 | 9.4 | 49.8 |  |  |  |  |
| $108^{\circ}$ | 7.01 | $42^{\circ}$ | 52.71 | 89.0 | 292 | 11.4 | 52.5 | 20.0 | 11.0 | 197- 292 | 600-890 |
| $108^{\circ}$ | 19.41 | $42^{\circ}$ | 52.21 | 215.0 | 705 | 14.6 | 58.2 | 19.2 | 10.5 | 66-705 | 200-2,150 |
| $108^{\circ}$ | 17.31 | $42^{\circ}$ | 52.21 | 120.0 | 394 | 12.9 | 55.2 | 17.8 | 9.8 | 98- 394 | 300- 1,200 |
| $108^{\circ}$ | 17.61 | $42^{\circ}$ | 50.51 | 180.6 | 592 | 14.1 | 57.3 | 19.6 | 10.8 | 164- 590 | 500-1,800 |
| $108^{\circ}$ | 17.31 | $42^{\circ}$ | 50.51 | 290.0 | 951 | 15.9 | 60.6 | 18.1 | 9.9 | 131- 394 | 400-1,200 |
| $108^{\circ}$ | 51.5' | $42^{\circ}$ | 50.21 | 60.0 | 197 | 9.5 | 49.1 | 30.6 | 16.8 | 33-164 | 100- 500 |
| $108^{\circ}$ | 52.81 | $42^{\circ}$ | 50.11 | 291.0 | 954 | 9.8 | 49.6 |  |  |  |  |
| $108^{\circ}$ | 9.51 | $42^{\circ}$ | 46.21 | 220.0 | 722 | 14.3 | 57.7 | 25.9 | 14.2 | 262- 722 | 800-2,200 |
| $107^{\circ}$ | 10.41 | $42^{\circ}$ | 45.41 | 1,410.0 | 4,625 | 62.1 | 143.7 | 39.0 | 21.4 | 328-4,625 | 1,000-14,100 |
| $107^{\circ}$ | 40.71 | $42^{\circ}$ | 45.41 | 41.0 | 134 | 8.7 | 47.6 | 11.8 | 6.5 | 66-134 | 200- 410 |
| $107^{\circ}$ | 40.71 | $42^{\circ}$ | 45.41 | 29.0 | 95 | 8.3 | 46.9 |  |  |  |  |
| $108^{\circ}$ | 40.71 | $42^{\circ}$ | 45.41 | 38.0 | 125 | 8.8 | 47.8 |  |  |  |  |
| $107^{\circ}$ | 10.71 | $42^{\circ}$ | 44.61 | 1,900.0 | 6,232 | 71.9 | 161.4 | 33.4 | 18.3 | 33-6,232 | 100-19,000 |
| $107^{\circ}$ | $35.4{ }^{1}$ | $42^{\circ}$ | 44.6' | 339.0 | 1,112 | 14.6 | 58.2 | 27.8 | 15.3 | 492- 689 | 1,500-2,100 |
| $107^{\circ}$ | 35.31 | $42^{\circ}$ | 44.51 | 340.0 | 1,115 | 14.6 | 58.2 | 21.5 | 11.8 | 492-1,115 | 1,500-3,400 |
| $107^{\circ}$ | 35.21 | $42^{\circ}$ | 44.0' | 232.0 | 761 | 14.9 | 58.8 | 38.7 | 21.2 | 66-492 | 200-1,500 |
| $107^{\circ}$ | 48.41 | $42^{\circ}$ | 41.91 | 127.0 | 417 | 10.1 | 50.1 | 20.2 | 11.1 | 164- 417 | 500-1,270 |
| $107^{\circ}$ | 48.51 | $42^{\circ}$ | 41.81 | 60.0 | 197 | 9.0 | 48.2 | 20.8 | 11.4 | 66- 197 | 200- 600 |
| $107^{\circ}$ | 48.3' | $42^{\circ}$ | 41.8' | 96.0 | 315 | 10.0 | 50.0 | 15.1 | 8.3 | 131-295 | 400- 900 |

Appendix A continued.

| Location |  | Depth |  | Bottom-hole Temperature ( ${ }^{\circ} \mathrm{C}$ ) ( ${ }^{\circ} \mathrm{F}$ ) |  | Gradient ${ }^{2}$${ }^{\circ} \mathrm{C} / \mathrm{km}{ }^{\circ} \mathrm{F} / 1,000$ |  | Interval ${ }^{3}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Longl tude | Latitude | Meters | Feet |  |  | Meters | Feet |
| $107^{\circ} 46.11$ | $42^{\circ} 40.71$ | 87.0 | 285 | 10.9 | 51.6 |  |  |  |  |  |  |
| $107^{\circ} 48.0^{\prime}$ | $42^{\circ} 40.4{ }^{\prime}$ | 65.0 | 213 | 10.8 | 51.4 | 45.2 | 24.8 | 66- 213 | 200- 650 |
| $107^{\circ} 44.31$ | $42^{\circ} 40.4{ }^{1}$ | 137.0 | 449 | 11.7 | 53.1 | 35.1 | 19.3 | 197-426 | 600-1,300 |
| $107^{\circ} 42.9{ }^{\prime}$ | $42^{\circ} 40.4{ }^{1}$ | 126.0 | 413 | 10.3 | 50.5 | 25.6 | 14.1 | 164-394 | 500- 1,200 |
| $107^{\circ} 42.0{ }^{\prime}$ | $42^{\circ} 40.4{ }^{1}$ | 177.0 | 581 | 12.0 | 53.6 | 31.6 | 17.3 | 98- 558 | 300-1,700 |
| $107^{\circ} 40.5{ }^{\prime}$ | $42^{\circ} 40.41$ | 127.0 | 417 | 10.0 | 50.0 | 22.4 | 12.3 | 164-417 | 500-1,270 |
| $107^{\circ} 42.9{ }^{1}$ | $42^{\circ} 39.4{ }^{\prime}$ | 203.0 | 666 | 12.0 | 53.6 | 26.1 | 14.3 | 131- 666 | 400- 2,030 |
| $107^{\circ} 41.9{ }^{\prime}$ | $42^{\circ} 39.4{ }^{1}$ | 180.0 | 590 | 14.4 | 57.9 | 54.2 | 29.8 | 131- 426 | 400- 1,300 |
| $107^{\circ} 40.61$ | $42^{\circ} 39.4{ }^{\prime}$ | 185.0 | 607 | 13.0 | 55.4 | 20.4 | 11.2 | 164- 525 | 500- 1,600 |
| $107^{\circ} 40.6{ }^{\prime}$ | $42^{\circ} 38.51$ | 216.0 | 708 | 13.6 | 56.4 | 40.3 | 22.1 | 295- 623 | 900- 1,900 |
| $107^{\circ} 40.61$ | $42^{\circ} 35.11$ | 255.0 | 836 | 12.5 | 54.5 | 26.4 | 14.5 | 230-623 | 700- 1,900 |
| $107^{\circ} 40.01$ | $42^{\circ} 35.0^{1}$ | 195.0 | 640 | 12.2 | 53.9 | 17.5 | 9.6 | 295- 525 | 900- 1,600 |
| $107^{\circ} 40.01$ | $42^{\circ} 35.0{ }^{\prime}$ | 180.0 | 590 | 12.2 | 53.9 | 20.9 | 11.5 | 262- 590 | 800- 1,800 |
| $107^{\circ} 40.01$ | $42^{\circ} 35.0^{1}$ | 57.0 | 187 | 9.8 | 49.6 | 13.5 | 7.4 | 66-187 | 200- 570 |
| $107^{\circ} 39.5{ }^{\prime}$ | $42^{\circ} 34.31$ | 310.0 | 1,017 |  | 55.9 |  | 10.1 | 295-820 | 900-2,500 |
| $107^{\circ} 56.21$ | $42^{\circ} 25.31$ | 1,310.0 | 4,297 | 59.6 | 139.2 | 38.7 | 21.2 | 131-4,297 | 400-13,100 |
| $107^{\circ} 56.41$ | $42^{\circ} 23.4{ }^{\prime}$ | 1,530.0 | 5,018 | 52.7 | 126.9 | 28.0 | 15.4 | 328-3,608 | 1,000-11,000 |
| Watrona County |  |  |  |  |  |  |  |  |  |
| $106^{\circ} 46.4^{\prime}$ | $42^{\circ} 51.41$ | 670.0 | 2,198 | 33.4 | 92.1 | 26.6 | 14.6 | 652-2,427 | 2,000-7,400 |
| $106^{\circ} 46.41$ | $42^{\circ} 51.4{ }^{1}$ | 380.0 | 1,246 | 24.3 | 75.7 | 33.3 | 18.3 | 66- 918 | 660-2,800 |

[^2]

Geology-Interpreting the past to proxide for the future


GENERALIZED GEOLOGIC MAP OF THE WIND RIVER BASIN, WYOMING


THERMAL GRADIENT CONTOUR MAP OF THE WIND RIVER BASIN, WYOMING


GENERALIZED STRUCTURE CONTOUR MAP ON THE TOP OF THE CLOVERLY FORMATION, WIND RIVER BASIN, WYOMING


TEMPERATURE CONTOUR MAP OF THE TENSLEEP SANDSTONE, WIND RIVER BASIN, WYOMING


[^0]:    Cover Photograph: Sweetwater Station Springs at the southern edge of the Wind River Basin. Two warm springs issue from alluvium deposited on Miocene Split Rock Formation. The site is at the intersection of an anticline and a fault. (Photograph by Bern S. Hinckley, from Thermal Springs of Wyoming, Geological Survey of Wyoming Bulletin 60, 1978).

[^1]:    ${ }^{1}$ Data condensed from Richter (1981) wIth modifications fran Whitcomb and Lowry (1968) and Love and Christiansen (1985),
    ${ }^{2}$ The quallty of water in any water-bearing strata may significantly deterlorate as the water migrates basinward.
    ${ }^{3}$ Termi nology from Love (1961), Pllocene rocks In the Granite Mountains.
    ${ }^{4}$ TDS $=$ total dissolved solids.
    ${ }^{5}$ Called Ar Ikaree Formation In Whitcomb and Lowry (1968).
    ${ }^{6}$ Called Park Clty Formation In RIchter (1981).

[^2]:    1 Measured by University of Wyoming personnel following the method of Decker (1973); data from Heasler and others (1983).

    2 Gradient represents a linear least squares fit of the temperature-depth data over the most thermally stable portion of the hole.

    3 Interval refers to the depth range over which the least squares gradient was calculated.

